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## Variance of the virtual displacement

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### Abstract

We show that the affine structure of the 3-dimensional space is deeply enmeshed with the static laws expression. The relevance of tensorial rules for calculus in mechanics is thus enhanced. The virtual work principle is stated precisely but a little twist is given to the usual statements: the tensorial nature of the so-called virtual displacement vector is asserted to be covariant. **To cite this article:** *C. Vallée et al., C. R. Mecanique 332 (2004).*

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### Résumé

**Variance du déplacement virtuel.** Nous montrons que la structure affine de l'espace tridimensionnel est fortement imbriquée avec l'expression des lois de la statique. La pertinence de l'application des règles du calcul tensoriel à la mécanique est ainsi renforcée. Le principe des travaux virtuels est établi précisément avec une seule entorse aux exposés classiques : la nature tensorielle de l'habituel vecteur déplacement virtuel est affirmée covariante. **Pour citer cet article :** *C. Vallée et al., C. R. Mecanique 332 (2004).*

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### Version française abrégée

Considérons  $N$  forces  $f_i$  (indexées de 1 à  $N$ ) appliquées en des points  $M_i$ . Les points  $M_i$  sont repérés par leurs trois coordonnées  $(x_i^1, x_i^2, x_i^3)$ , les forces  $f_i$  sont évaluées par leurs trois composantes  $(f_i^1, f_i^2, f_i^3)$ . Elle sont en équilibre si :

$$\begin{aligned} \sum_{i=1}^N f_i^1 = 0 \quad \sum_{i=1}^N f_i^2 = 0 \quad \sum_{i=1}^N f_i^3 = 0 \\ \sum_{i=1}^N (x_i^2 f_i^3 - f_i^2 x_i^3) = 0 \quad \sum_{i=1}^N (x_i^3 f_i^1 - f_i^3 x_i^1) = 0 \quad \sum_{i=1}^N (x_i^1 f_i^2 - f_i^1 x_i^2) = 0 \end{aligned}$$

Les 3 premières conditions expriment que la résultante des forces est nulle et les 3 dernières que leur moment résultant est aussi nul. Si on introduit des champs  $z_j$  du type :

$$z_j(x^1, x^2, x^3) = t_j + \sum_{k=1}^3 \omega_{jk} x^k$$

(où les  $t_j$  et les  $\omega_{jk}$  sont des scalaires,  $\omega_{kj} = -\omega_{jk}$ ), alors les 6 lois de la statique se résument en

$$\sum_{i=1}^N \sum_{j=1}^3 z_j(x_i^1, x_i^2, x_i^3) f_i^j = 0$$

Il se trouve que les champs  $z_j$  sont caractérisés par le système linéaire d'équations aux dérivées partielles

$$\frac{\partial z_j}{\partial x^k} + \frac{\partial z_k}{\partial x^j} = 0$$

Un nouvel énoncé du principe de la statique est donc :

$$\frac{\partial z_j}{\partial x^k} + \frac{\partial z_k}{\partial x^j} = 0 \quad \Rightarrow \quad \sum_{i=1}^N \sum_{j=1}^3 z_j(x_i^1, x_i^2, x_i^3) f_i^j = 0$$

On reconnaît le principe des travaux virtuels en interprétant les champs  $z_j$  comme les composantes d'un déplacement virtuel et la somme

$$\sum_{i=1}^N \sum_{j=1}^3 z_j(x_i^1, x_i^2, x_i^3) f_i^j$$

comme le travail virtuel des forces  $f_i$ . Nous montrons que cet énoncé du principe des travaux virtuels n'est indépendant du choix des coordonnées que si les changements de variables autorisés sont affines. Ainsi se trouvent fortement imbriquées la structure de l'espace et l'invariance par changement de coordonnées des lois de la statique. La seule entorse aux exposés classiques du principe des travaux virtuels est la nature tensorielle du déplacement virtuel qui est affirmée covariante plutôt que contravariante.

### 1. Balance of forces and moments

Let us consider  $N$  forces  $f_i$  (indexed by  $i$  from 1 to  $N$ ) applied in  $N$  points  $M_i$ . On the mathematical level, we only will know at this beginning, as in the remote time of Archimedes [1] and Euclid, but with notations of today [2], that:

- a point  $M_i$  can be located by 3 coordinates  $x_i^1, x_i^2, x_i^3$ ,
- a force  $f_i$  applied in  $M_i$  can be evaluated by 3 components  $f_i^1, f_i^2, f_i^3$ .

On a mechanical level, what Archimedes said, and after him Simon Stevin [3], was the conditions for what  $N$  forces  $f_i$  are in equilibrium. These conditions can be expressed by 6 formulae readable for an engineer knowing only what are the coordinates of a point and what are the components of a force:

$$\sum_{i=1}^N f_i^1 = 0 \quad \sum_{i=1}^N f_i^2 = 0 \quad \sum_{i=1}^N f_i^3 = 0 \tag{1}$$

$$\sum_{i=1}^N (x_i^2 f_i^3 - f_i^2 x_i^3) = 0 \quad \sum_{i=1}^N (x_i^3 f_i^1 - f_i^3 x_i^1) = 0 \quad \sum_{i=1}^N (x_i^1 f_i^2 - f_i^1 x_i^2) = 0 \tag{2}$$

The 3 first conditions constitute the so-called resultant force law of static, and the 3 last the even so-called resultant moment law. We can already notice that these equations are written without needing any notion of dot product, or cross product, or angle. Up to this point, the mathematical structure of the space is intentionally poor, what we want precisely is to discover its fair geometry for the sake of static modeling. Better than invoking a posteriori the Ockam razor principle [4], we will seek the minimal properties satisfied by the changes of coordinates insuring the permanence of the 6 static laws expression.

### 2. First static laws summary

Let us multiply respectively, the 3 first conditions by 1-indexed scalars  $t_1, t_2, t_3$ , the 3 last ones by 2-indexed scalars  $\omega_{32}, \omega_{13}, \omega_{21}$ , understood to be skew-symmetrical, and let us add all of them. Then the 6 conditions ((1), (2)) synthesize in

$$\sum_{i=1}^N \left( \sum_{j=1}^3 \left( t_j + \sum_{k=1}^3 \omega_{jk} x_i^k \right) f_i^j \right) = 0$$

Also, we can summarize all static laws by: “ $N$  forces  $f_i$ , applied in  $N$  points  $M_i$ , are in equilibrium if

$$\sum_{i=1}^N \sum_{j=1}^3 z_j(x_i^1, x_i^2, x_i^3) f_i^j = 0$$

for any testing field  $z_j$  of the type

$$z_j(x^1, x^2, x^3) = t_j + \sum_{k=1}^3 \omega_{jk} x^k \tag{3}$$

with  $\omega_{kj} = -\omega_{jk}$ ”.

### 3. Characterization of testing fields

We can remark [5] the characterization:

$$z_j(x^1, x^2, x^3) = t_j + \sum_{k=1}^3 \omega_{jk} x^k \Leftrightarrow \frac{\partial z_j}{\partial x^k} + \frac{\partial z_k}{\partial x^j} = 0$$

### 3.1. Direct property

The direct property is obvious because in this case the partial derivative  $\frac{\partial z_j}{\partial x^k} = \omega_{jk}$  is skew-symmetrical, and then its symmetrical part is null. What happens is that the converse is true.

### 3.2. Converse property

Let us assume  $\frac{\partial z_j}{\partial x^k}$  to be skew-symmetrical, therefore its first derivative  $\xi_{jkl} = \frac{\partial}{\partial x^l} \frac{\partial z_j}{\partial x^k}$  is symmetrical with respect to the 2 last indexes as any good second derivative and remains skew-symmetrical with respect to the 2 first ones. However, the braids lemma [6] afterward mentioned says that this is possible only when  $\xi_{jkl}$  is null. Then, it is very straightforward to achieve the proof of the converse property: each derivative  $\omega_{jk} = \frac{\partial z_j}{\partial x^k}$  does not depend of the coordinates  $x^1, x^2, x^3$ ; and it is easy to integrate in (3).

### 3.3. Braids lemma

“If  $\xi_{jkl}$  is symmetrical with respect to the 2 last indexes and skew-symmetrical with respect to the 2 first ones, then  $\xi_{jkl}$  is null”.

**Proof in 6 strokes.** The scalar  $\xi_{jkl}$  is opposite to itself  $\xi_{jkl} = -\xi_{kjl} = -\xi_{klj} = \xi_{lkj} = \xi_{ljk} = -\xi_{jlk} = -\xi_{jkl}$  and so is null.

## 4. Second static laws summary

“ $N$  forces  $f_i$ , applied in  $N$  points  $M_i$ , are in equilibrium if

$$\sum_{i=1}^N \sum_{j=1}^3 z_j(x_i^1, x_i^2, x_i^3) f_i^j = 0$$

for any testing field  $z_j$  solution of

$$\frac{\partial z_j}{\partial x^k} + \frac{\partial z_k}{\partial x^j} = 0$$

## 5. Consistency

One question arises: is this second summary, coordinate free? More precisely, if new coordinates  $y^1, y^2, y^3$  are chosen, does this formulation perpetuate? To answer to this, we may have an idea about how change the components  $f^j$  and  $z_j$  of respectively a force and a testing field. We only will remember [2] of what precedes that the space is a 3-dimensional manifold  $V$  and we will assume that:

- the components  $f^j$  of a force  $f$  change locally as the coordinates, they become  $F^j = \sum_{k=1}^3 \frac{\partial y^j}{\partial x^k} f^k$  using the partial derivatives  $\frac{\partial y^j}{\partial x^k}$  of the new coordinates with respect to the old ones,
- the old components  $z_j$  of the testing field are replaced by new ones  $Z_j$  in accordance with the rule  $z_j = \sum_{k=1}^3 \frac{\partial y^k}{\partial x^j} Z_k$  insuring a common meaning to  $\sum_{j=1}^3 Z_j F^j$  and  $\sum_{j=1}^3 z_j f^j$ .

The question now is: do the new components  $Z_j$  remain solutions of  $\frac{\partial Z_j}{\partial y^k} + \frac{\partial Z_k}{\partial y^j} = 0$ ?

Thus we come to our main result.

## 6. Allowable changes of coordinates

“The changes of coordinates consistent with the static laws expressed by our second summary are the affine ones

$$y^j = \sum_{k=1}^3 A_k^j x^k + b^j \quad (4)$$

where the  $A_k^j$  and the  $b^j$  are respectively the coefficients of an invertible  $3 \times 3$  matrix and a  $3 \times 1$  matrix”.

**Proof.** The 2 assumptions are

$$(1) \quad z_j = \sum_{k=1}^3 \frac{\partial y^k}{\partial x^j} Z_k \quad (2) \quad \frac{\partial z_j}{\partial x^k} + \frac{\partial z_k}{\partial x^j} = 0 \Leftrightarrow \frac{\partial Z_j}{\partial y^k} + \frac{\partial Z_k}{\partial y^j} = 0$$

Thanks to the first assumption, the symmetrical parts of the first derivatives of  $z_j$  and  $Z_j$  are related by

$$\frac{\partial z_j}{\partial x^k} + \frac{\partial z_k}{\partial x^j} = \sum_{l=1}^3 \left( \frac{\partial}{\partial x^k} \frac{\partial y^l}{\partial x^j} + \frac{\partial}{\partial x^j} \frac{\partial y^l}{\partial x^k} \right) Z_l + \sum_{l=1}^3 \sum_{m=1}^3 \frac{\partial y^l}{\partial x^j} \left( \frac{\partial Z_l}{\partial y^m} + \frac{\partial Z_m}{\partial y^l} \right) \frac{\partial y^m}{\partial x^k}$$

Thanks to the second assumption

$$\sum_{l=1}^3 \left( \frac{\partial}{\partial x^k} \frac{\partial y^l}{\partial x^j} \right) Z_l = 0$$

may hold, in particular, for constants  $Z_l$ . As a consequence, all the second derivatives  $\frac{\partial}{\partial x^k} \frac{\partial y^l}{\partial x^j}$  are null, and it is easy to integrate in (4).

## 7. Affine space

The allowable changes of coordinates are correlated with the action of an affine group on the space. We do believe that the geometry is given by the acting group as Felix Klein claimed in his Erlangen Program [7], therefore the manifold  $V$  is no more than an affine space. In this space, coming from sake of Archimedes static, the relevant notion is the parallelism. We emphasized on coordinates and changes of coordinates rather than on basis or changes of basis, nevertheless all axiomatic definitions of affine and linear spaces can be rebuilt.

## 8. Virtual work principle

Our second summary of static is nothing else than the virtual work principle [8]. The only twist we gave to the classical statements is that we have evaluated a force  $f$  by its effect when submitted to a linear form  $z$ . This effect  $\sum_{j=1}^3 z_j f^j$  is the virtual work. Following the Ockam economy principle [4], we will prefer such an evaluation to the usual one by a dot product with a so-called virtual displacement vector, because we did not encounter any natural argument for a metric in our modeling of static.

The type  $t_j + \sum_{k=1}^3 \omega_{jk} x^k$  of that kind of ‘covariant virtual displacement’  $z_j$  recalls the type of classical rigid body virtual displacement vectors:

- the part of small translations is played by  $t_j$ ,
- the part of small rotations is played by  $\omega_{jk}$ .

But  $\omega_{jk}$  has not any interpretation through a small rotation because there is no metric in the affine space. In such a space, nobody is able to define what is a rigid body.

## 9. Conclusion

Archimedes and Euclid were contemporary. It seems that they established simultaneously the foundations of static and geometry with common words [9,10]. Our result tells that the affine structure of the 3-dimensional space is self-consistent with the expression of static laws.

The linear group associated to the affine group acts on the linear space  $E$  associated to the affine space. The good rules for calculating in  $E$  are those of tensorial calculus introduced at the beginning of the XXth century by Gregorio Ricci-Curbastro and Tullio Levi-Civita. Rules for calculating in the affine space are not so well-known, the understanding of the mechanical situation will be improved by considering specially the geometry generated by the affine group and by introducing ‘affine’ tensors [11] in competition with the classical ‘linear’ tensors.

There is no need for a metric when speaking about the equilibrium of a system of forces. This lack of natural metric in the affine space leads to give up to rotations. Therefore, the notion of rigid body displacement vector is lost and so is the characterization by the vanishing of the self-adjoint part of its derivative. However, the ‘covariant virtual displacements’  $z_j$  satisfying  $\frac{\partial z_j}{\partial x^k} + \frac{\partial z_k}{\partial x^j} = 0$  reveal themselves to be as much fruitful [12,13,7] for generalizations to continuum media and applications to strength of materials.

Moreover, extending the covariant virtual displacements  $z_j$  to the four dimensional affine space-time provides dynamics of rods and shells as well as dynamics of three dimensional media [14,11].

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